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腐蚀-荷载耦合作用下不锈钢结构性能研究进展

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摘 要: 不锈钢结构凭借其出色的防腐性能及良好的力学特性在工程领域受到越来越广泛的关注, 然而不锈钢在极端环境中其性能依然存在劣化现象, 深入探究不锈钢结构在腐蚀-荷载耦合作用下的性能演化是推动其工程应用的重要前提。从材料-结构层面梳理了国内外关于不锈钢在腐蚀环境中的力学性能研究成果, 揭示了包括点蚀、应力腐蚀和疲劳腐蚀在内的不锈钢腐蚀特点, 总结分析了腐蚀环境钢结构力学性能劣化规律, 概括论述了腐蚀环境钢结构寿命评估方法, 最后提出了当前研究体系存在的问题。通过对研究进展的梳理, 可以看出国内外学者在相关领域已取得丰富的研究成果, 但仍存在不足。国内外已有研究主要集中在对不锈钢材料腐蚀行为的分析上, 并未提出能够反映腐蚀状态下不锈钢应力-应变关系曲线的本构模型, 难以有效解释由材料到结构层面的腐蚀传递机制。已有研究均以碳钢材料为对象开展腐蚀-荷载作用下的失效行为分析, 针对不锈钢结构力学性能劣化缺乏研究积累, 此外针对荷载作用下结构性能的损伤研究不够深入, 无法有效揭示不锈钢结构承载力的退化规律。本构模型和结构性能研究的不足使得基于时变可靠度方法定量分析结构抗力退化缺少充足的输入变量样本数据, 进而导致对腐蚀环境中不锈钢结构服役寿命的评估体系不完整, 耐久性设计缺乏技术支撑。

关键词: 桥梁不锈钢; 腐蚀-荷载耦合; 结构性能; 性能劣化; 寿命评估; 综述

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Research progress on the performance of stainless steel structures under corrosion-load coupling effects

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Abstract: Stainless steel structures have gained increasing attention in the field of engineering due to their excellent corrosion resistance and favorable mechanical properties. However, stainless steel exhibits performance degradation under extreme environmental conditions. Investigating the performance evolution of stainless steel structures under corrosion-load coupling conditions is an essential prerequisite for advancing their broader engineering applications. This study systematically reviews the domestic and international research on the mechanical performance of stainless steel in corrosive environments from both material and structural perspectives. It elucidates the characteristics of stainless steel corrosion, including pitting corrosion, stress corrosion, and fatigue corrosion. Additionally, it summarizes and analyzes the degradation patterns of mechanical properties of steel structures exposed to corrosive environments, discusses methodologies for evaluating the service life

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of steel structures under corrosion, and identifies existing issues within the current research framework. Through this review, it becomes apparent that global scholars have achieved substantial research outcomes in this field, yet significant gaps remain. Most existing studies focus on analyzing the corrosion behavior of stainless steel materials but fail to propose constitutive models that accurately reflect the stress-strain relationship of stainless steel under corrosive conditions. This gap hinders a comprehensive explanation of the corrosion transmission mechanisms from the material to the structural level. Furthermore, previous research primarily centers on carbon steel materials when analyzing failure behaviors under corrosion-load coupling conditions. Consequently, there is a lack of accumulated research on the mechanical performance degradation of stainless steel structures. Studies investigating the damage to structural performance under load are also insufficient, which makes it challenging to reveal the degradation laws of the load-bearing capacity of stainless steel structures effectively. The inadequacies in constitutive modeling and structural performance research result in a shortage of adequate input data for quantitative analyses of structural resistance degradation by using time-variant reliability methods. This limitation compromises the comprehensiveness of service life evaluation systems for stainless steel structures in corrosive environments and undermines the technical foundation for designing durable structures.

Key words: stainless steel for bridge; corrosion-load coupling; structural performance; performance degradation; life evaluation; review

腐蚀所致的金属构件破损降低了结构的强度,同时所产生的锈迹亦会加速腐蚀进程从而导致结构整体性能的严重损伤。我国拥有西太平洋最长的海岸线,沿线分布着数量庞大的基础设施,它们即将进入腐蚀破坏的高风险期,并严重威胁结构的安全,显著增加维护成本。据调查统计^[1],早在2014年我国腐蚀成本就已经达到了21 278.2亿元人民币,约占当时我国GDP的3.34%,相当于每位公民承担的腐蚀成本超过了1 555元。因此,提高海洋环境中基础设施的耐久性和安全性,降低灾害性事故的发生率,延长这些重大工程设施的使用寿命,是我国经济发展中需要迫切解决的问题。

近年来,不锈钢材料凭借其美观、耐腐蚀以及显著的应变硬化效应等优点在工程领域中受到越来越多的关注。相比于普通碳钢和低合金钢,不锈钢的这些独特的材料特性使其能够在恶劣环境中依然表现优异。因此,在海洋环境中采用不锈钢结构比采用普通钢结构更能有效地解决金属腐蚀问题,也是提升沿海结构服役寿命的关键,而且全寿命周期成本分析证明不锈钢比普通钢更具有优势^[2-3]。事实上,世界范围内已有68座桥梁整体或部分使用了不锈钢作为结构材料。随着沿海新基建需求的增加,更多设施结构有望采用不锈钢材料,如海上风机、跨海大桥、海上漂浮结构以及悬浮

隧道等。国内外学者通过对不锈钢材料进行腐蚀研究后发现,其力学性能同样存在劣化现象,尤其是当其暴露在腐蚀-荷载工况下时,而海岸线的基础设施正处于这种复杂环境中,其中荷载因素可包括车、风、浪等。如何准确评估这种多交互、强耦合因素对不锈钢结构力学性能的影响,是海洋环境中不锈钢结构应用亟须解决的关键问题。目前,关于不锈钢受力性能的研究仅涉及荷载因素,并未考虑腐蚀-荷载联合作用的影响,致使研究成果难以反映复杂环境中不锈钢受力性能的劣化现象。推动海洋环境中不锈钢结构应用的另一个关键问题是如何准确预测不锈钢结构的服役寿命。当前对腐蚀环境中不锈钢结构性能退化规律研究的不足导致相应的寿命预测缺乏基础数据支撑。从结构全寿命角度出发,提高腐蚀环境中不锈钢结构寿命的预测精度不仅能够确保沿海基础设施结构的安全,同时可以实现整体经济成本的控制,对不锈钢结构工程的可持续发展具有重要的现实意义和社会价值。

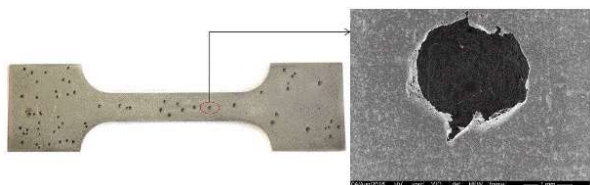
为此,本文对不锈钢材料在腐蚀环境中的性能研究进行了归纳总结,分类阐述了不锈钢的腐蚀特点,同时分析了腐蚀环境中钢结构力学性能劣化规律,对腐蚀钢结构寿命评估方法进行了概括论述,进而为不锈钢结构腐蚀的研究提供研究思路。

1 不锈钢材料腐蚀行为研究

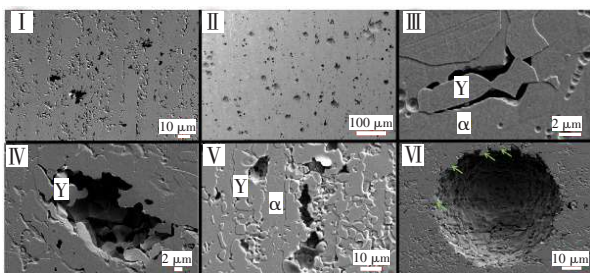
海洋环境中不锈钢材料的腐蚀形态通常表现为点蚀和缝隙腐蚀^[4],其与荷载耦合后将进一步产生应力腐蚀^[5]以及疲劳腐蚀^[6]。国内外学者分别就不锈钢的腐蚀形态和破坏模式展开了大量研究。

1.1 不锈钢点蚀

点蚀是在不锈钢表面局部形成的具有一定深度的小孔或锈斑,尽管肉眼难以观察,却显著影响材料的性能。在实验室可以通过快速腐蚀试验生成不锈钢点蚀试件进而定量研究腐蚀形态^[7-8],如图1所示。文献[9-11]通过对点蚀成核与扩展过程的追踪,揭示了该类腐蚀的发展规律,并深入探究了影响不锈钢腐蚀的关键因素。这些因素包括:①温度。高温会加速不锈钢表面点蚀的发生和发展过程,增大电化学反应速率并降低钝化膜的稳定性,从而降低材料的耐蚀性。②pH值。酸性环境使钝化膜破坏加剧,即较低的pH值会加剧不锈钢点蚀。③氯化物浓度。氯化物浓度的增加能够促进阳极反应,进而明显提升不锈钢的点蚀敏感性。



(a) 不锈钢试件点蚀^[7]



注:α为铁素体;Y为奥氏体。

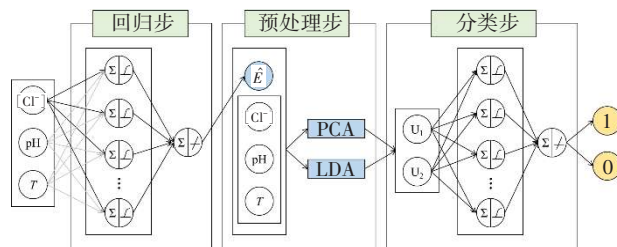
(b) 点蚀形貌发展过程^[8]

图1 不锈钢点蚀形态

Fig. 1 Pitting corrosion

然而受限于试验规模与经济成本,上述测试通常仅聚焦于较为单一的腐蚀环境,难以结合多种环境变量生成丰富的试验数据。因此,部分学者在现有数据的基础上利用数学模型、有限元模型以及神经网络等模拟了点蚀过程。XIE等^[12]提出了一种基于物理的多状态马尔可夫数学模型,该模型能够描述点蚀的各个状态,通过试验数据校正,实现了对

不同环境中点蚀深度和密度变化的模拟。JAFARZADEH等^[13]归纳总结了不锈钢点蚀的计算模型并分析了多个计算模型的优缺点。点蚀模型可分为非自主模型和自主模型两类,非自主模型包括使用有限元方法求解传输方程和点蚀边界的演化;自主模型则通过整合腐蚀前沿的溶解反应动力学和电解液中的离子传输动力学,实现腐蚀坑的自主增长。JIMÉNEZ-COME等^[14]提出了如图2所示的一种基于人工神经网络(artificial neural network, ANN)的三步骤模型,旨在克服电化学测试或腐蚀微观分析的局限性,该模型获得了较为满意的精度。需要指出的是,上述研究一般没考虑荷载的耦合作用。



注:PCA指主成分分析;LDA指线性判别分析; T 为温度; $\hat{E}$ 为电势; U_1 、 U_2 均为分类结果的类别标签。

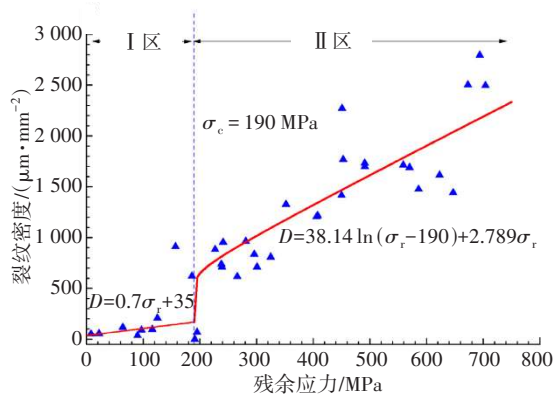
图2 基于ANN的三步骤模型^[14]

Fig. 2 Three-stage model based on ANN^[14]

1.2 不锈钢应力腐蚀

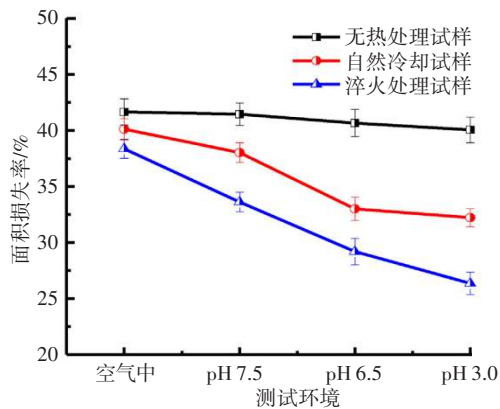
引入荷载后,不锈钢在拉应力与腐蚀介质的共同作用下将会发生应力腐蚀开裂,并以裂纹萌生、扩展、断裂为标志^[15]。该类破坏在发生前金属表面未见明显塑性变形,属于脆性断裂,无法充分利用不锈钢延性大的优势,且破坏危害大。为此,国内外学者利用试验和数值模拟手段对不锈钢应力腐蚀开裂进行了过程研究。ZHU等^[16]通过试验、有限元模拟以及电镜扫描分析了在超低弹性载荷下不锈钢点蚀和早期应力腐蚀开裂的萌生和初期阶段的特征,发现点蚀主要起始于样品表面并沿厚度方向快速扩展,该现象同样得到了SPENCER等^[17]的研究论证。FUJII等^[18]利用衍射技术对奥氏体不锈钢应力腐蚀开裂(stress corrosion cracking, SCC)早期阶段的成核行为进行了详细分析,探讨了微观结构特征对SCC成核的影响。此外,文献[19-21]研究了表面光滑度、残余应力、酸性等因素的影响(如图3所示),同时在晶体微观层面分析了破坏机理,发现在腐蚀和外荷载的共同作用下在晶界附近晶体出现了较大的晶间应力,导致晶间出现滑移裂纹,使得金属内部重新暴露于腐蚀环境中,并重复晶间滑

移过程。其中所采用的最普遍的测试方法为低应变速率法^[22],常用的应变速率为 $10^{-7} \sim 10^{-5} \text{ s}^{-1}$ 。



注: σ_c 为残余应力临界值; σ_r 为表面残余应力; D 为表面裂纹密度。

(a) 残余应力对应力腐蚀的影响^[19]

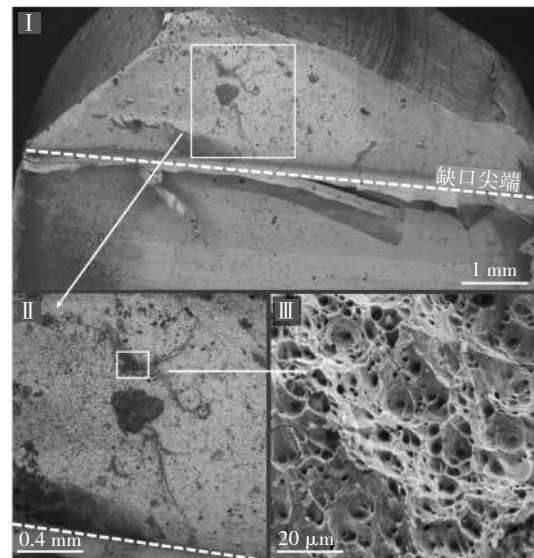


(b) 酸性环境对应力腐蚀的影响^[20]

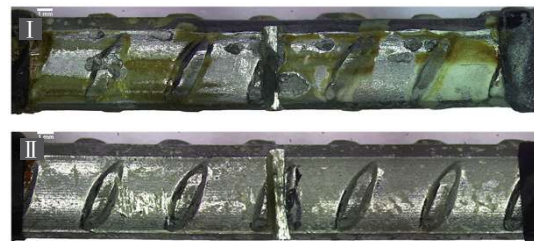
图3 不锈钢应力腐蚀影响因素分析

Fig. 3 Effect analysis on stress corrosion of stainless steel

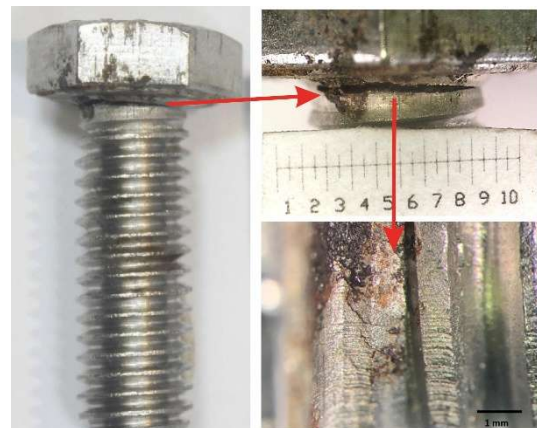
近几年,对不锈钢应力腐蚀开裂的研究开始转向钢筋和螺栓等部件(如图4所示)。MARTIN等^[23]和BRIZ等^[24]利用电化学方法模拟混凝土孔隙中含氯离子溶液的腐蚀,分别研究了奥氏体不锈钢钢筋和双相不锈钢钢筋的应力腐蚀开裂机理。GONZÁLEZ-VELÁZQUEZ等^[25]对由海洋环境中氯离子所导致的304型号不锈钢螺栓的应力腐蚀、开裂失效进行了断裂力学分析。通过分析失效螺栓的断裂韧性、裂纹扩展速率及应力强度因子等参数,揭示了氯离子应力腐蚀的开裂机理,并讨论了材料性能、应力水平等因素对应力腐蚀开裂的影响。值得注意的是,研究发现,如果螺栓在安装过程中承受了超出名义夹紧载荷1.55倍的紧固应力,将会加速腐蚀裂纹的萌生和扩展。然而上述研究仅对腐蚀速率与裂纹状态进行了描述,并指出了裂纹发展与应力强度因子之间的关系,但受限于材料强度,研究成果难以应用于工程结构的设计中。



(a) 奥氏体不锈钢钢筋腐蚀微观形貌^[23]



(b) 双相体不锈钢钢筋腐蚀形貌^[24]



(c) 不锈钢螺栓应力腐蚀^[25]

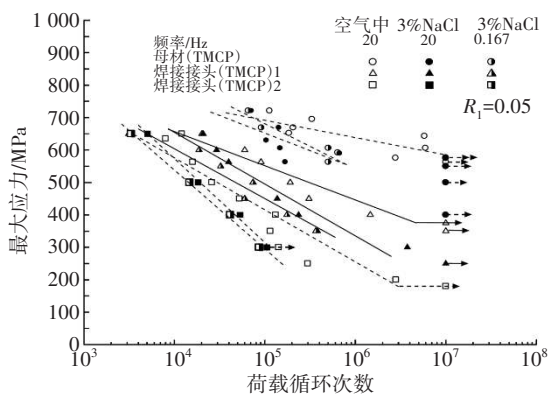
图4 不锈钢钢筋及螺栓应力腐蚀开裂

Fig. 4 Stress corrosion crack of stainless steel reinforcements and bolts

1.3 不锈钢腐蚀疲劳

不锈钢腐蚀疲劳是由交变应力和腐蚀介质共同作用产生的破坏模式,与一般机械疲劳相比,腐蚀疲劳的不锈钢表面常见明显的腐蚀^[26]。目前,已有大量文献研究了不锈钢腐蚀疲劳裂纹的形成和扩展机制、扩展速率以及各种因素对 $S-N$ 曲线(应力-疲劳寿命曲线,其中 S 为应力, N 为荷载循环次数)的影响^[26-38]。EBARA^[26]系统地总结了包括马氏

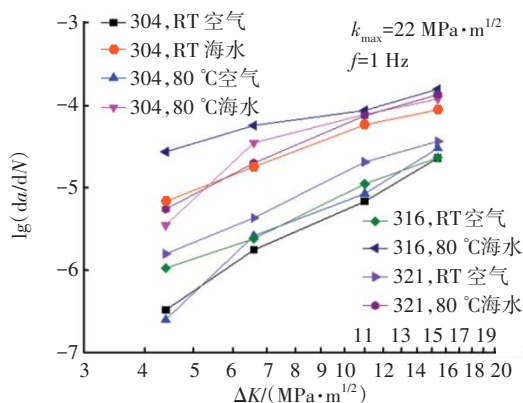
体、铁素体、奥氏体和双相不锈钢腐蚀疲劳裂纹的萌生机制(如图5所示),指出对于工程应用较多的奥氏体和双相不锈钢,其抗腐蚀疲劳强度相对较高,同时冶金因素与双相不锈钢腐蚀疲劳裂纹的萌生机理关系密切。范镒等^[6]通过开展海水环境中奥氏体不锈钢腐蚀疲劳试验进一步分析了裂纹的扩展行为,并基于Paris公式拟合出了腐蚀疲劳裂纹扩展曲线,如图6所示。杨斌等^[34]对2205型号双相不锈钢腐蚀疲劳裂纹的扩展进行了同类试验研究(如图7所示),通过Paris公式拟合发现海水环境中该类材料的裂纹扩展速率较大气环境中显著提高,疲劳寿命显著降低。值得注意的是,目前腐蚀疲劳研究均是从不锈钢材料出发而并未涉及疲劳细节。



注:TMCP为热机械控制工艺; R_1 为残差。

图5 基材与焊接节点在空气与3%NaCl溶液中的S-N曲线^[26]

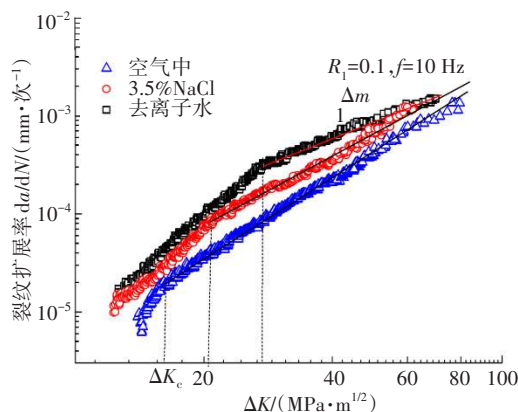
Fig. 5 S-N diagrams of base metal and welded joints in air and in 3%NaCl aqueous solution^[26]



注: $k_{\max}$ 为最大应力强度因子; f 为加载频率; ΔK 为应力强度因子幅值; a 为裂纹扩展长度;RT指室温。

图6 3种奥氏体不锈钢(304、316、321)的疲劳裂纹扩展速率^[6]

Fig. 6 Fatigue crack growth rate of 304, 316, and 321 stainless steel^[6]



注: ΔK_c 为应力强度因子临界值; Δm 为线性拟合参数。

图7 3种环境中2205型号双相不锈钢的应力强度因子幅值与裂纹扩展速率关系曲线^[34]

Fig. 7 Relationship between stress intensity factor amplitude and fatigue crack growth rate of 2205 duplex stainless steel under three environments^[34]

2 腐蚀环境中钢结构力学性能劣化研究

从材料层面对不锈钢腐蚀行为进行研究所积累的丰富成果为不锈钢结构性能劣化探索建立了良好的开端,然而目前深入到结构层面的研究非常匮乏。为此,本节从本构关系-构件性能角度归纳总结腐蚀环境中碳钢结构性能退化的研究现状,旨在为不锈钢材料的研究提供研究思路和方法。

在工程结构分析中,本构关系是评估结构性能的重要参考依据,建立不同腐蚀时间、腐蚀程度的不锈钢应力-应变关系曲线是分析不锈钢结构性能劣化的基础。SHENG等^[39]开展了点蚀作用下碳钢拉伸性能试验,并考虑了蚀坑形状、深度以及分布的影响,研究表明腐蚀后的极限荷载与最小截面面积相关(如图8所示),而屈服强度受蚀坑形状、深度与密度的影响。然而,ZHAO等^[40]通过参数有限元模型模拟计算了随机点蚀下Q345钢材的强度,发现用最小截面面积确定极限强度偏于保守,并提出了基于质量损失率和蚀坑深度的强度公式(如图9所示,图中上下两条粗线分别是由极限强度数据和屈服强度数据拟合得到的幂函数曲线)。WANG等^[41]将质量损失率和坑蚀径深比等参数应用到了预测Q355B钢的腐蚀强度上。

REN等^[42]利用单轴拉伸试验和有限元模拟研究了不同点蚀参数对腐蚀钢材力学性能的影响(如图10所示),指出点蚀区域中最明显的腐蚀缺陷与钢材性能的削弱有直接关系。张浩^[43]进一步简化

了腐蚀钢材力学模型,建立了最大蚀坑影响系数与力学性能之间的定量关系,并基于二次屈服退化模型拟合得到了腐蚀状态下的强度曲线。KONG等^[44]在试验数据的基础上对比分析了既有腐蚀强度预测模型的精度,并基于 Hollomon 模型提出改进方法预测 Q235 和 Q355 钢的应力-应变曲线。可以看出,目前对腐蚀后碳钢力学性能的退化规律已积累了大量研究成果,所建立的材料力学性能退化模型在不锈钢材料上的应用值得借鉴。

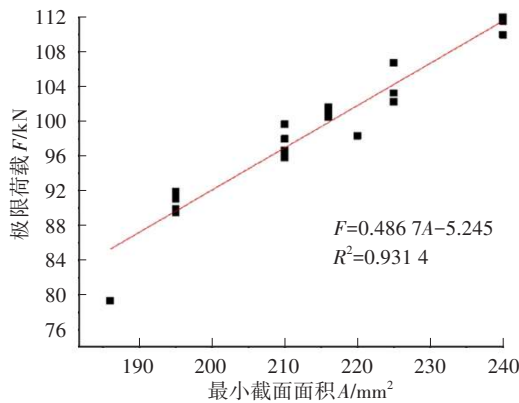
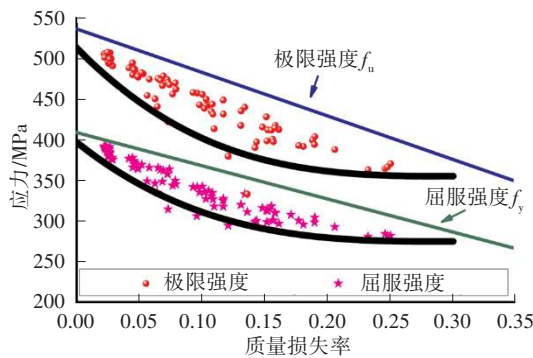
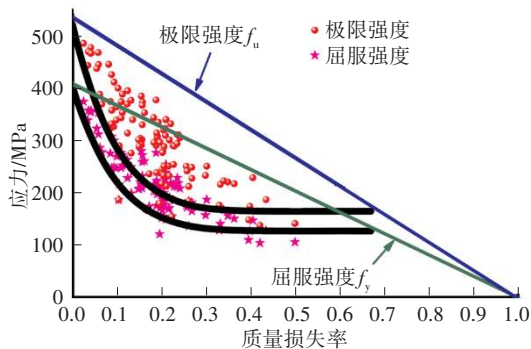


图8 极限荷载与最小截面面积的关系^[39]

Fig. 8 Relationship between ultimate load and minimum section area^[39]



(a) 蚀坑相对深度 0.15 ~ 0.35



(b) 蚀坑相对深度 0.15 ~ 0.85

图9 拉伸强度与质量损失率、蚀坑深度的关系^[40]

Fig. 9 Relationship of tensile strength with mass loss rate and corrosion depth^[40]

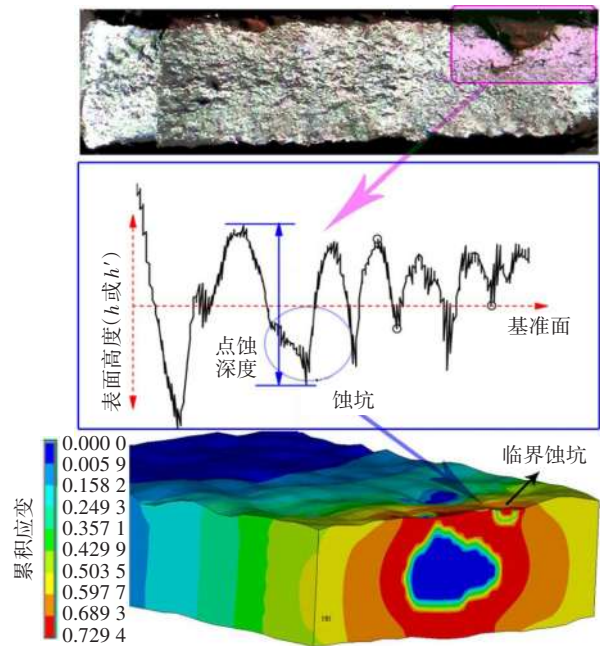


图10 腐蚀缺陷对钢材性能的影响^[42]

Fig. 10 Effect of corrosion defects on the material property of steel^[42]

在腐蚀环境中构件由于受到拉压弯剪等的作用会出现不同的性能劣化现象,国内外学者为此分别针对梁、柱、连接节点等构件形式开展了大量研究^[45-58]。其中,SHENG等^[45]对10组“工”字形钢梁进行腐蚀-弯矩耦合测试后发现,随着腐蚀率的增加,梁的极限承载力显著下降,荷载-位移曲线呈现出三个阶段,即弹性阶段、屈服硬化阶段和承载力退化阶段。ZHAO等^[48]通过数值模拟分析了“工”字形钢梁在点蚀随机分布状态下的抗剪性能,确定了蚀坑深度与质量损失率对结构承载力的影响,并提出了适用于长细比小于1的“工”字形钢梁的残余抗剪强度模型。陈尧^[51]通过均匀腐蚀和随机点蚀开展了34根轴心受压构件的局部和整体稳定性试验,并基于有限元参数化分析建立了以平均腐蚀率、腐蚀延伸和构件正则化长细比为影响指标的承载力随时间变化的退化模型。类似地,LI等^[52]研究了局部点蚀破坏下钢管混凝土柱的稳定性能(如图11所示),并提出了能预测腐蚀后钢管混凝土柱强度的简化公式:

$$N_{pro} = A_c f_c + \gamma A_s f_y \quad (1)$$

$$\gamma = 2.36 - 5.44 \rho_l \rho_h \quad (2)$$

式中: N_{pro} 为腐蚀后钢管混凝土柱的承载力; A_c 和 A_s 分别为核心混凝土和钢管的横截面面积; f_c 为未被约束的混凝土的抗压强度; γ 为被腐蚀钢结构的承载力折减系数; ρ_l 和 ρ_h 分别为沿深度和高度方向的

腐蚀水平。

需要强调的是,由于不锈钢与碳钢力学性能的差异(不锈钢具有高延性及明显应变硬化的特点),针对碳钢的研究方法可以作为参考,但不能完全照搬并应用于不锈钢的研究中。



图11 试验腐蚀试件^[52]

Fig. 11 Corroded specimens in test^[52]

3 被腐蚀钢结构寿命评估方法研究

钢结构构件在外荷载和腐蚀的共同作用下,其结构性能随着时间的推移逐渐劣化,进而影响了结构的服役寿命。准确评估不锈钢结构在海洋环境中的服役寿命是推动不锈钢材料广泛可靠地应用在沿海基础设施工程中的关键。目前,关于不锈钢寿命评估的文献仅集中在上述不锈钢材料的腐蚀疲劳方面,此类研究成果难以支撑腐蚀-荷载共同作用下构件层面的寿命预测。本节归纳总结以碳钢为对象的研究现状,旨在为未来不锈钢结构寿命的评估提供技术思路。

钢结构在荷载-腐蚀环境中性能的变化过程属于时域动态非线性过程且具有不确定性^[59-61],因此寿命评估也应基于时变可靠度方法对结构抗力的退化规律进行定量分析。当前,随着可靠度分析方法的发展,逐步形成了基于概率论的 Monte Carlo 法、随机有限元法以及神经网络法。ADUMENE 等^[62]研究了海洋腐蚀环境中结构多重失效模式及其相互依赖性对系统安全性和可靠性的影响。通过构建混合模型,结合 Monte Carlo 模拟,分析腐蚀作用下多种物理化学参数及其与失效模式之间的动态相互作用(如图 12 所示)。研究表明该方法能够预测腐蚀速率,评估失效概率。此外,多位学者^[63-67]利用 Monte Carlo 法模拟了随机腐蚀下梁柱等

结构的可靠度并提出了时变可靠度预测方法,然而该方法的精度与样本容量呈正相关关系,因此计算成本通常较高。随机有限元法将有限元分析与概率设计技术相结合,在有限元模型的基础上定义腐蚀-荷载随机输入变量,通过循环分析生成响应指标并对其进行失效概率计算,该方法被广泛应用在海洋腐蚀环境中管道构件的寿命评估中^[68-70]。事实上,随机有限元法在面对复杂模型时同样面临计算量大的问题,而近年来发展起来的神经网络法在大样本多参数方面能够有效克服上述时变可靠度分析中的问题。张振浩等^[71]通过建立后向传播(back propagation, BP)神经网络模型对钢箱梁腐蚀疲劳时变可靠性进行了分析,为既有钢桥腐蚀疲劳寿命的评估提供了新的方法。DANG 等^[72]通过时变可靠度案例分析对比了贝叶斯神经网络法和 Monte Carlo 法的效率和精度,研究发现神经网络法在计算

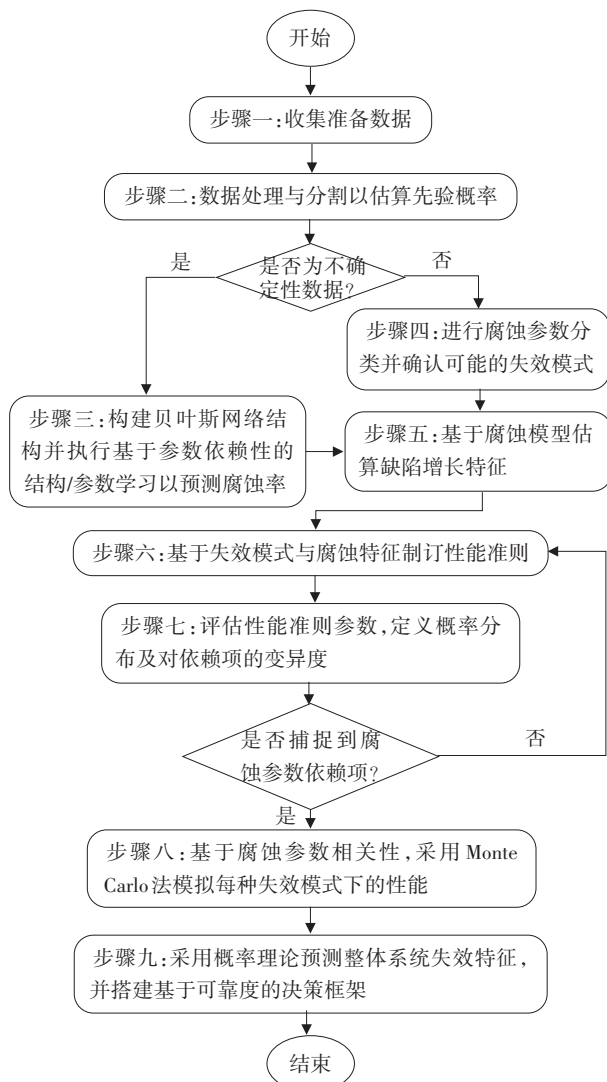


图12 混合方法流程图^[62]

Fig. 12 Flowchart of hybrid methodology^[62]

效率上比 Monte Carlo 法快三个数量级。ALAMRI^[73]通过文献综述提出了基于机器学习算法的应力腐蚀开裂寿命评估框架,并强调了该方法在算力以及成本上的优势。进一步地,FENG 等^[74]利用改进的深度卷积神经网络对海洋焊接结构的腐蚀疲劳寿命进行了评估,该方法使评估结果的精度提高了80%以上。

4 结论

纵观国内外已有研究,海洋腐蚀环境中不锈钢性能劣化已引起了广泛关注,国内外学者在相关领域已取得了丰富的研究成果。本研究从不锈钢材料腐蚀行为、腐蚀环境中钢结构力学性能劣化以及被腐蚀钢结构寿命评估方法三个方面对文献进行了调研,结论如下:

1) 腐蚀环境中不锈钢力学本构模型尚不完备。国内外已有研究主要集中在不锈钢材料腐蚀行为的分析上,聚焦在表面形貌特征以及裂纹萌生扩展规律的描述上,并未提出能够反映腐蚀状态下不锈钢应力-应变关系曲线的本构模型,难以有效解释由材料到结构层面的腐蚀传递机制;针对不同的腐蚀环境类型,尚未归纳总结各个类型下有代表性的腐蚀参数对力学本构模型的影响,对后续结构性能分析及寿命评估无法提供理论基础。

2) 关于腐蚀-荷载交互作用下不锈钢结构力学性能的劣化缺乏研究积累。已有研究均以碳钢材料为对象开展腐蚀-荷载作用下结构的失效行为分析,然而碳钢与不锈钢在材料性能和力学模型上的差异使得碳钢的研究成果难以支撑不锈钢结构的设计,在实践中存在局限性;针对荷载作用下结构性能的损伤研究不够深入,无法有效揭示不锈钢结构承载力的退化规律。

3) 对海洋腐蚀环境中不锈钢结构的寿命评估不足,缺乏设计依据,使得使用时变可靠度方法定量分析结构抗力的退化缺少充足的输入变量样本数据,进而导致对海洋腐蚀环境中不锈钢结构服役寿命的评估体系不完整,耐久性设计缺乏技术支撑,阻碍了不锈钢结构在沿海地区的应用。

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